



# Optimization of coupling between Adaptive Optics and Single Mode Fibers

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Non common path aberrations compensation through dithering

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ONERA

THE FRENCH AEROSPACE LAB

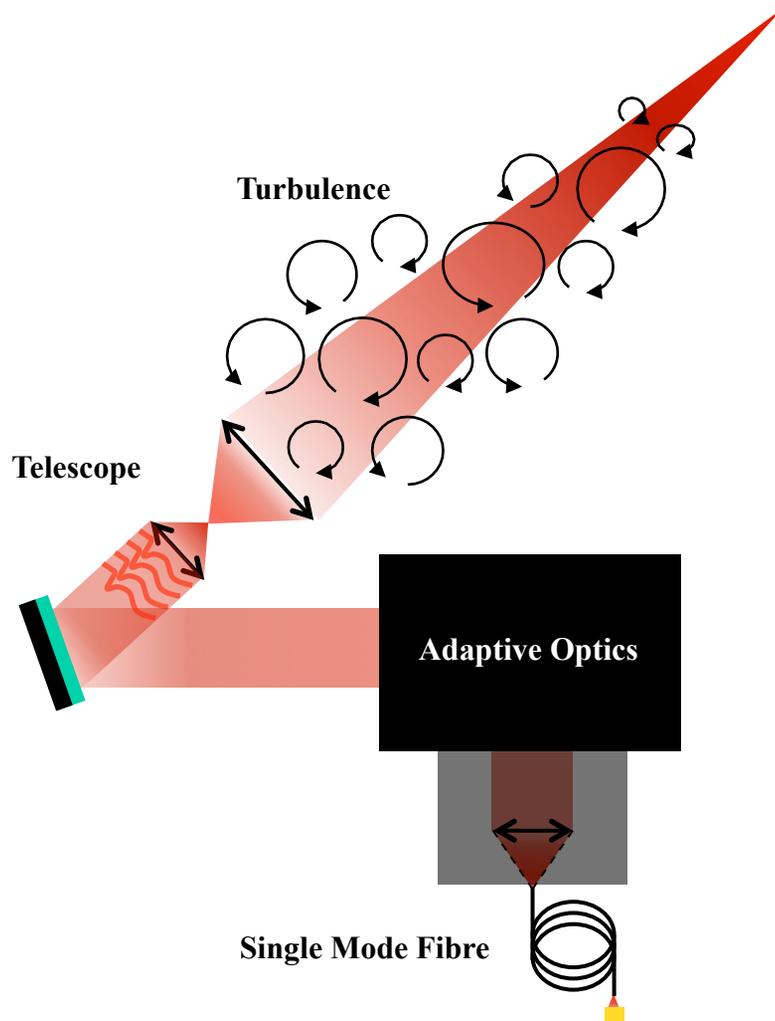


retour sur innovation

# Outline

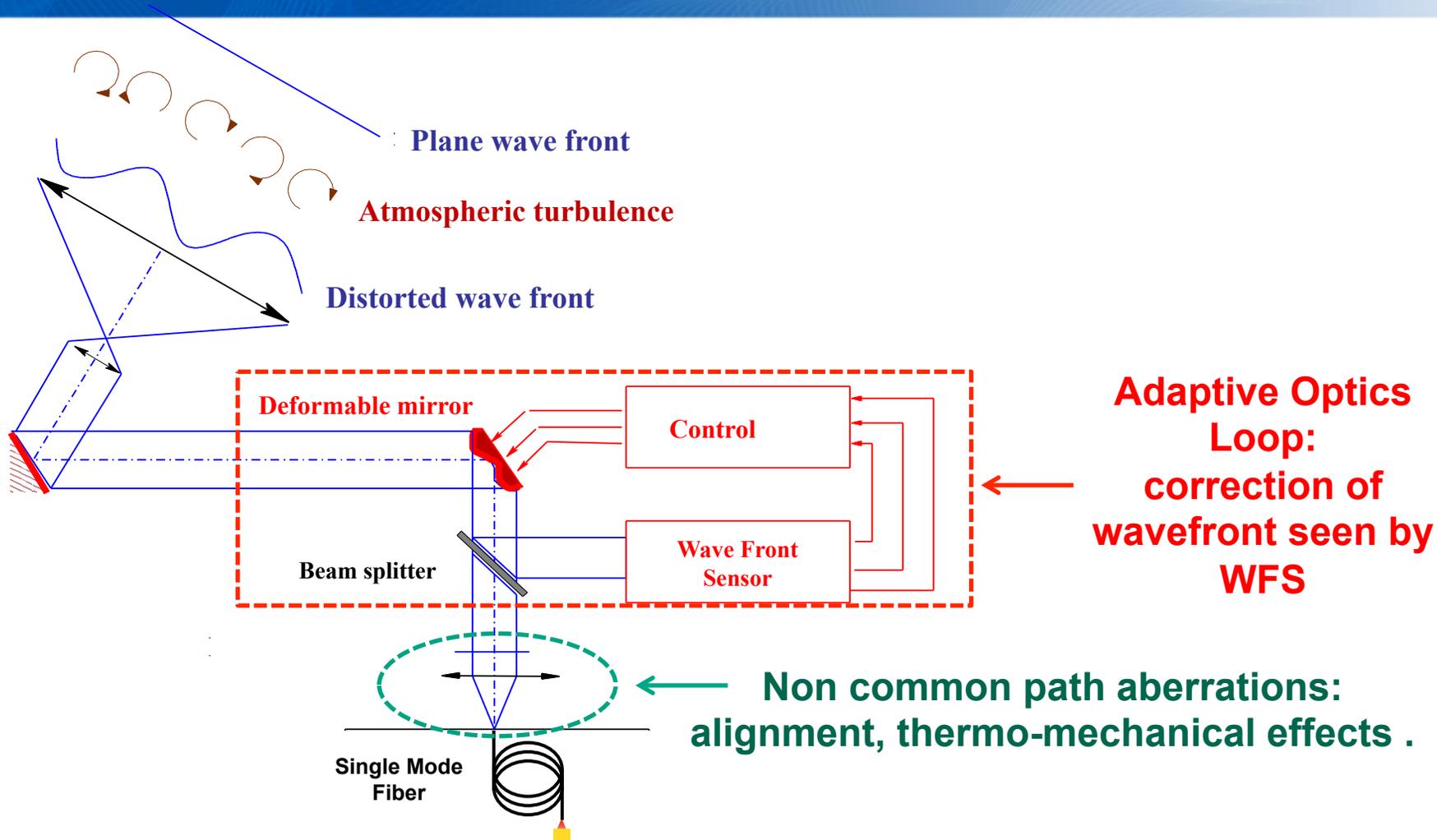
- ❑ Problem statement
- ❑ Concept
- ❑ Results
- ❑ Conclusions

# Context



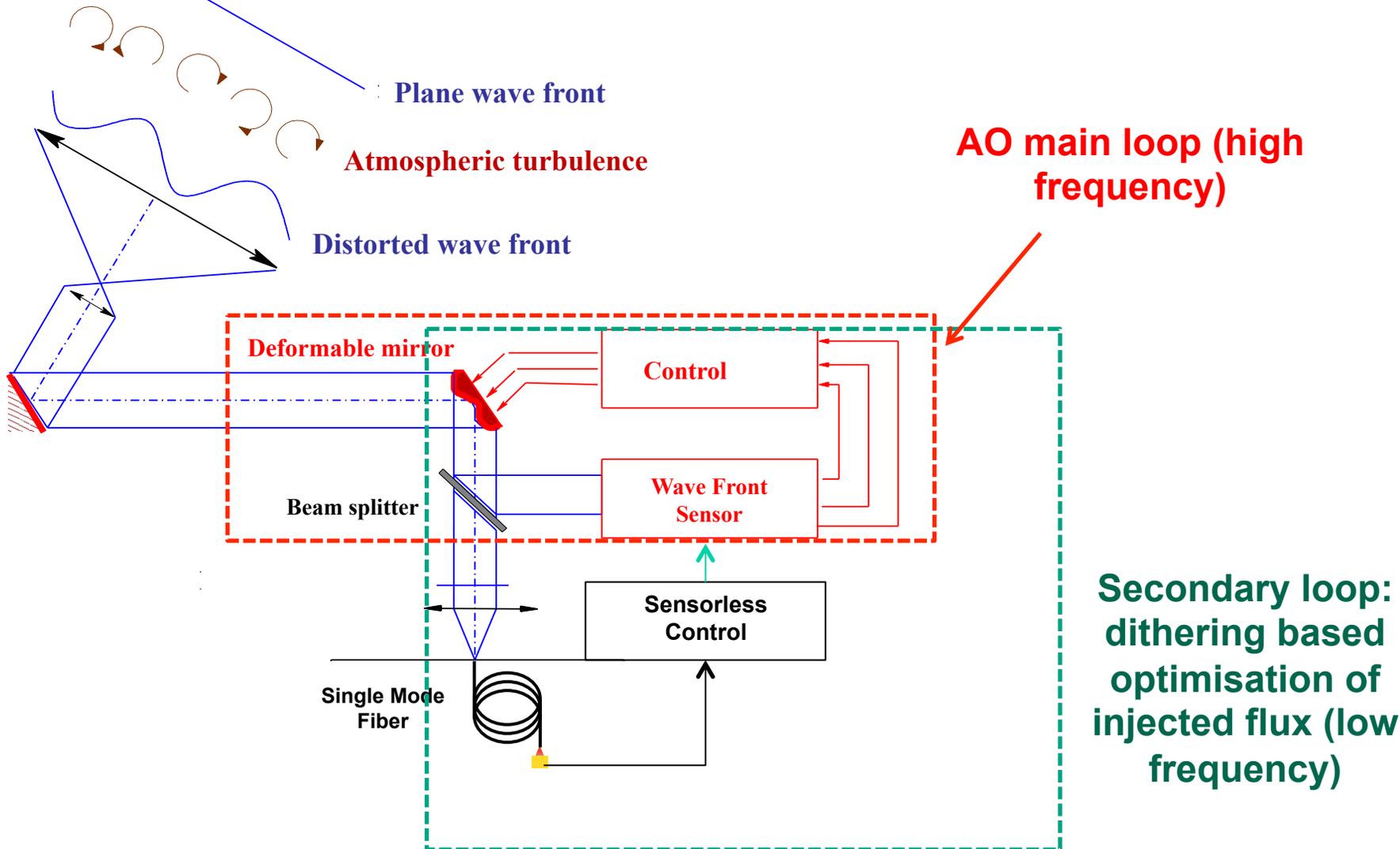
- Long baseline optical interferometry, Space-to-ground Optical Communications
- Injection of optical signal into SMF
- Use of AO for correction of atmospheric turbulence induced perturbations

# Problem statement



***Correction of wavefront injected into SMF ?***

# Problem statement

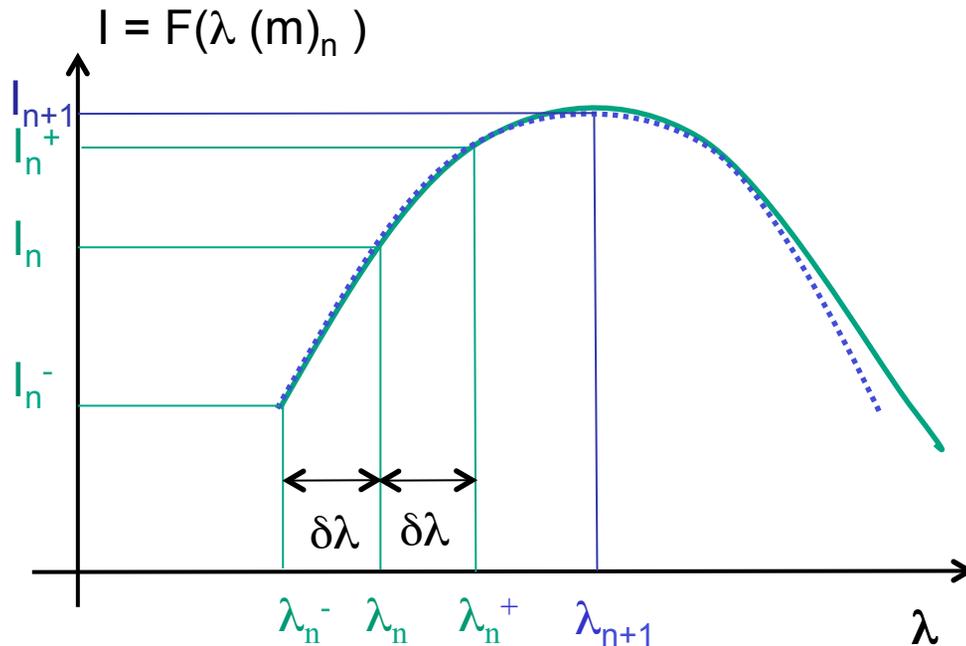


# Concept of « sensorless » loop

- Single measurement (coupled flux), Multi dimension correction using AO deformable mirror => use of dithering
  - Correction through AO: can only be introduced by modification of setpoint = reference slopes
  - From control point of view: Cascade control
    - Main AO loop ( $f_s > 100$  Hz)
    - « sensorless » loop ( $f_s \# 1$  Hz)
- => Modifications of DM shape introduced by the « sensorless » loop can be seen as quasi-static by the main AO loop (modification of setpoint of AO): temporal decoupling
- « sensorless » loop:
    - Control in the AO loop eigen modes:  $(m)$  ;
    - Application of sensorless loop control onto DM  $(v)$  by projection of modes  $(m)$  onto reference slopes  $(\delta p)$  of WFS:  $(\delta p) = A(m)$  then  $(v) = D(\delta p)$  ( $D =$  AO command Matrix);
    - Iterative search of maximum along random directions of the eigen modes space  $(m)_n$ .
    - Principle : dithering with parabolic fit. Can be related to Stochastic Parallel Gradient Descent (SPGD)

# Optimization by dithering

*Coupling efficiency  $I$  in one direction of modulation  $(m)_n$*



$\lambda_n$  amplitude on mode  $(m)_n$   
 $I_n$  associated coupling efficiency

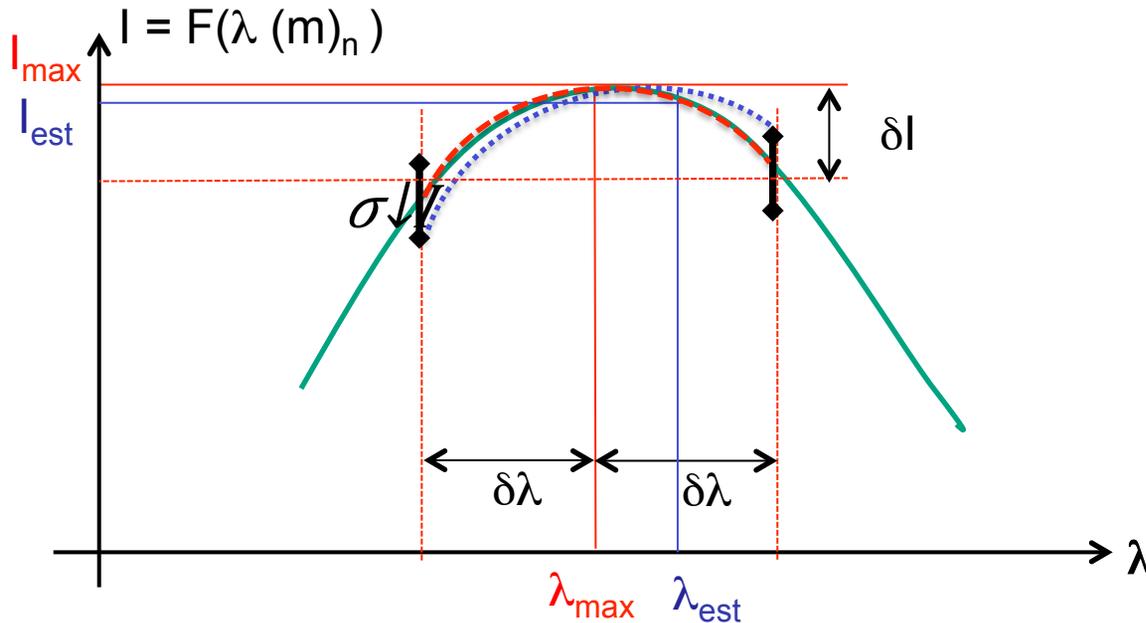
Choice of direction of modulation  
 in eigen mode space  $(m)_n$ ,

For that direction:

- Modulation of amplitude  $\pm \delta\lambda$   
 in mode space,
- Detection of associated signals  
 $I_n^+$ ,  $I_n^-$ ,
- Determination of maximum by  
 parabolic fit,  $\lambda_{n+1}$
- Conversion into slopes of  
 associated mode vector and  
 detection of output signal.

# Impact of noise

Coupling efficiency  $I$  in one direction of modulation  $(m)_n$



Modulation of amplitude  
 $\pm \delta\lambda$  in mode space  
 $\pm \delta I$  in coupling efficiency

Internal source  
 $\sigma \downarrow I \rightarrow$  Detection noise

External source  
 $\sigma \downarrow I \rightarrow$  Turbulence

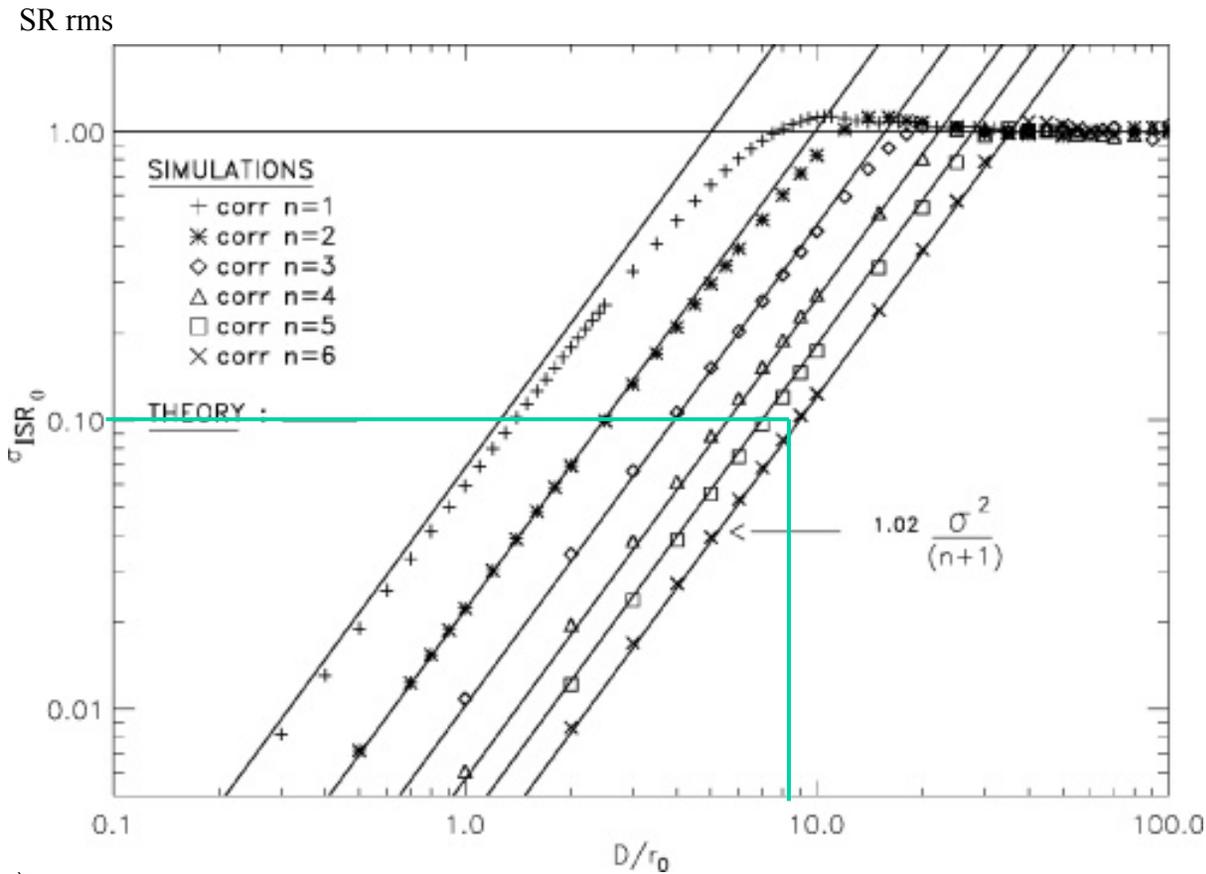
$$\text{Attenuation : } \langle I \downarrow_{max} - I \downarrow_{est} \rangle / I \downarrow_{max} = 1/8$$

$$\left( \frac{\sigma I}{I_{max}} \right)^2 \approx 2 I \downarrow_{max} / dI$$

- Reduction of  $\sigma \downarrow I$  : temporal averaging of coupled signal
- Increase of  $\delta I$  : increase of modulation amplitude  $\delta\lambda$  in mode space

# Optimization on sky with AO

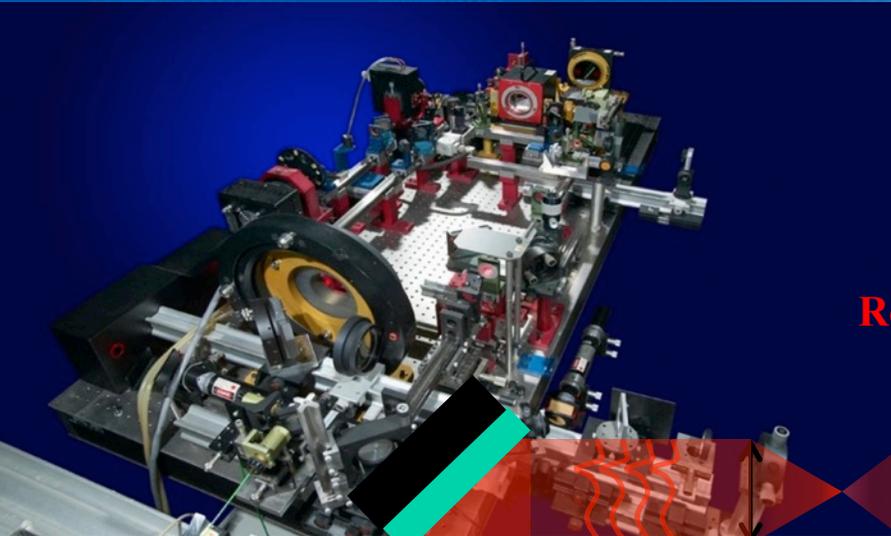
*fitting error limited AO case*



Thierry Fusco and Jean-Marc Conan, "On- and off-axis statistical behavior of adaptive-optics-corrected short-exposure Strehl ratio," *J. Opt. Soc. Am. A* **21**, 1277-1289 (2004)

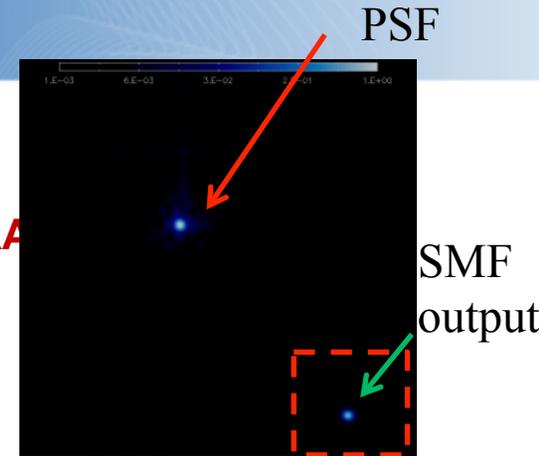
- Assume modulation:  
 $I \downarrow_{max} / dI = 0,1$
- Consider  $\langle \frac{I}{I} \rangle = 0,1$
- then  $\langle I \downarrow_{max} - I \downarrow_{est} \rangle / I \downarrow_{max} = 0,01$

# Experimental validation in the lab

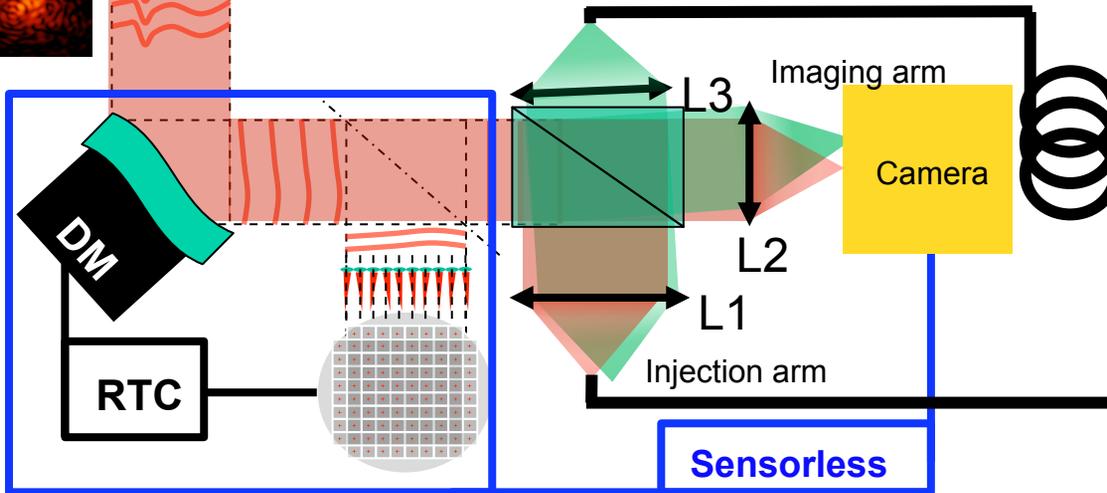
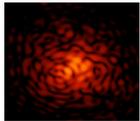


BOA bench @ONERA

Rotating phase screens



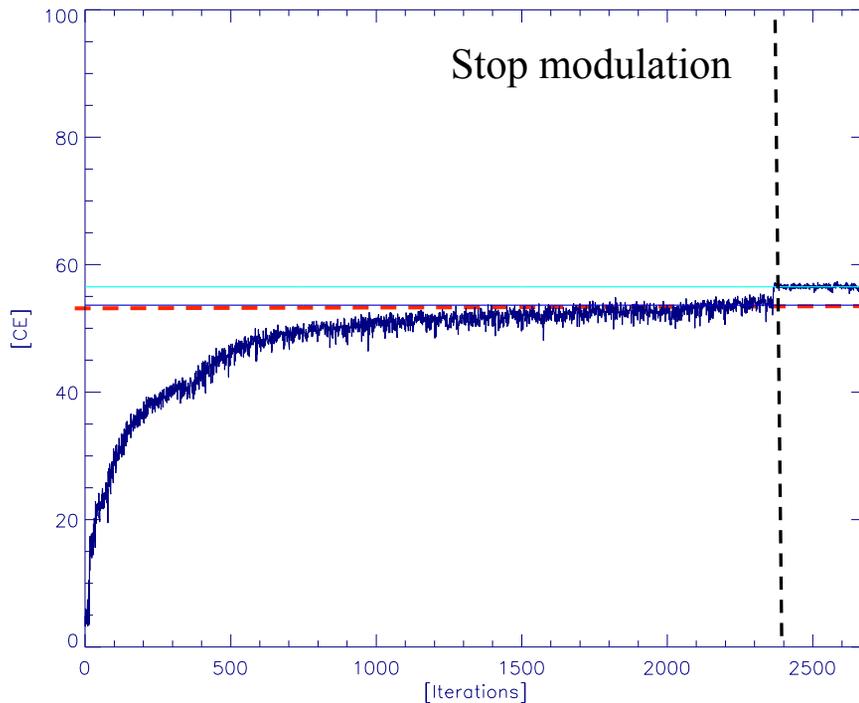
internal source @ 635 nm



SAAB, workshop Chara 2016, Nice

# Experimental validation in the lab: no turbulence case

## Convergence of CE optimisation



56% CE

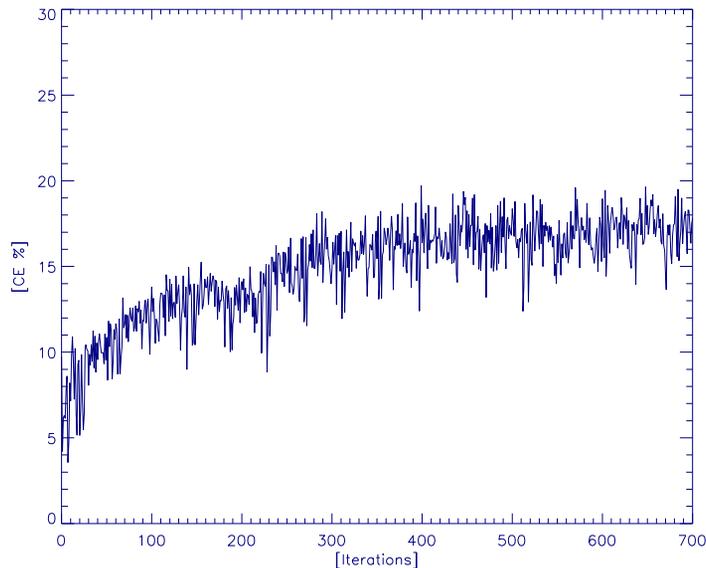
Itérations stands for each modulation

- Optimisation of static aberrations.
- Can be performed with input source (no use for intermediate reference source as in AO)
- Convergence speed not critical.

# Experimental validation in the lab: turbulent case

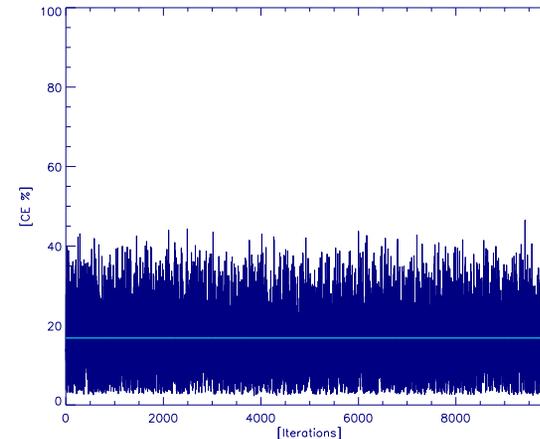
- Turbulence ON

Convergence of CE optimisation

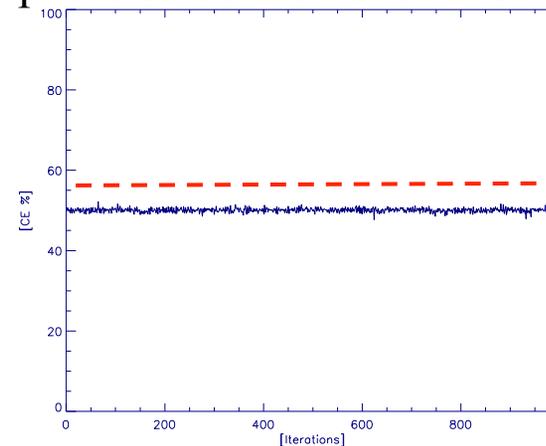


Residuals mainly driven by AO performance !

Stability after convergence



If phase screen removed ? Sensorless loop stopped



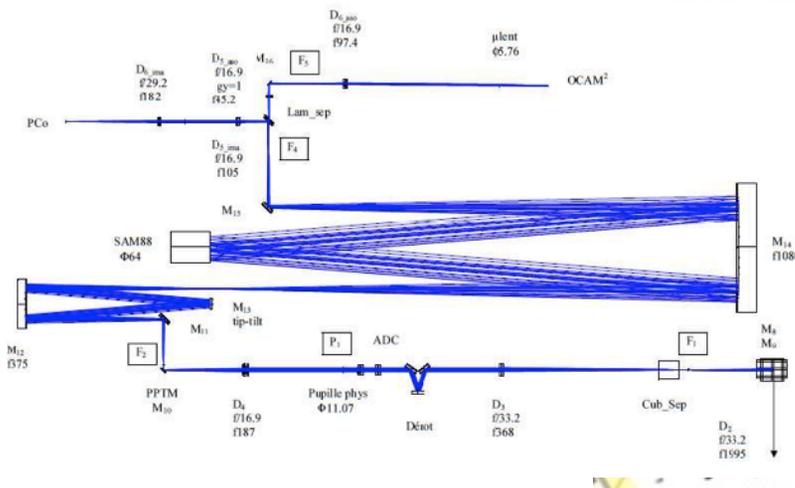
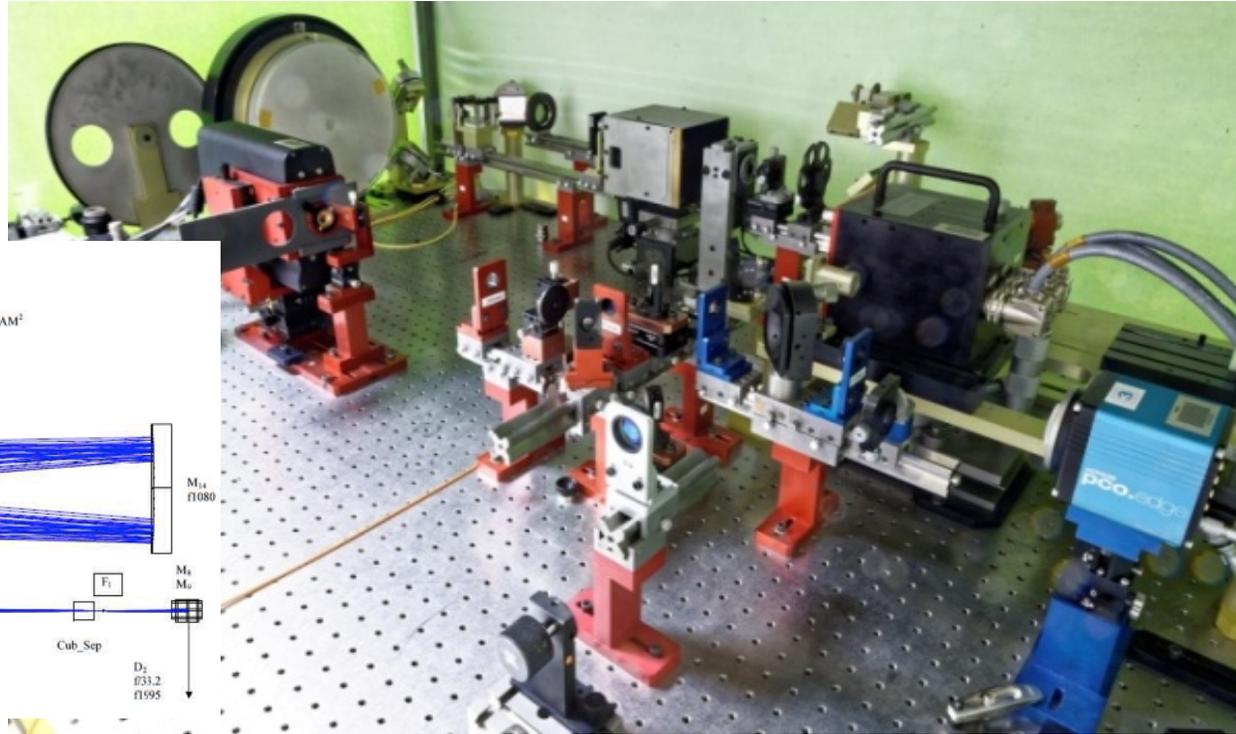
No turb: 56% CE

PS removed: 50% CE

convergence speed and performance as fonction of number of actuators, amplitude of modulation, averaging to be analyzed

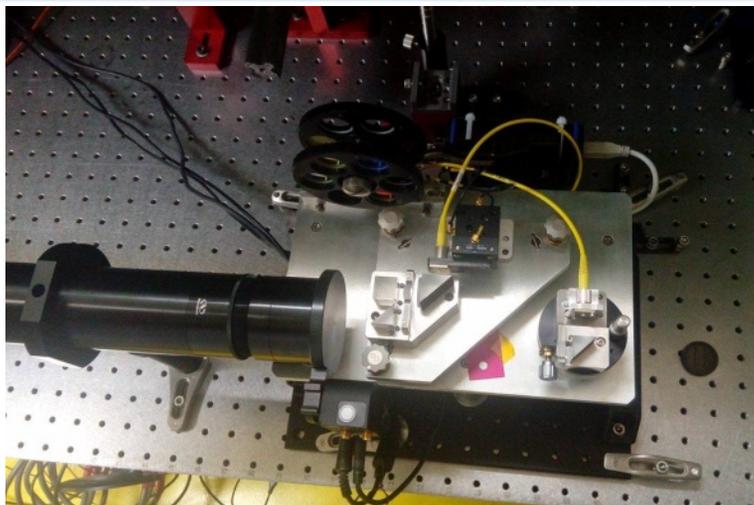
# AO bench ODISSEE @ OCA

90 actuators  
8x8 SH-WFS  
Up to 1.5kHz

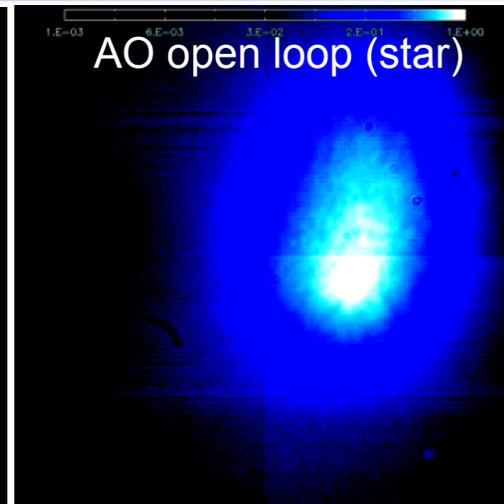
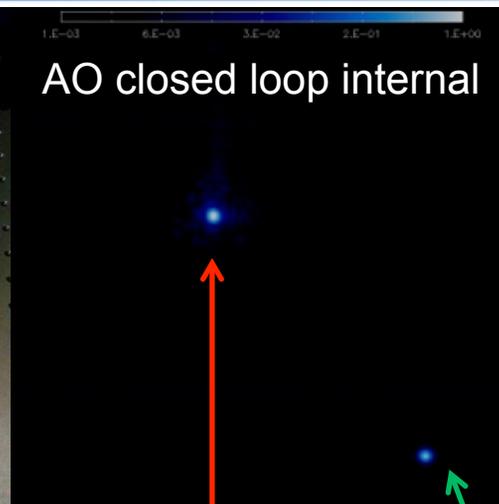


Validation of hybrid AO on ODISSEE ( $D = 1,5 \text{ m}$ , 8x8 sous-pupilles, 1500 Hz)  
**CESAR mission:** coupling of star light into SMF for long baseline interferometry (collaboration : ONERA/Lagrange).  
**SOTA/SOCRATES mission:** coupling of telecom signal into SMF (collaboration : ONERA/CNES/NICT/OCA).

# CESAR preliminary results (star @ 700 nm)



Cesar Module from Lagrange

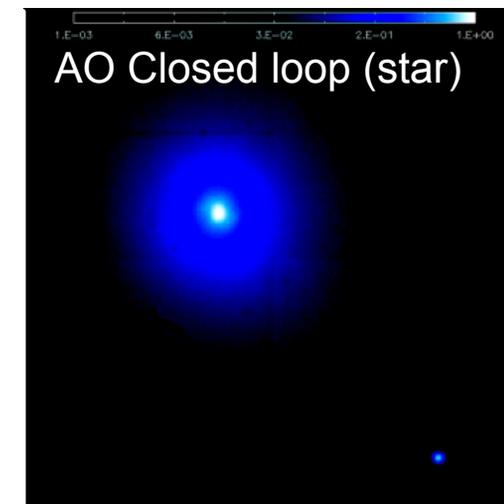


PSF from AO and SMF output image optically combined onto the same detector

Static (internal source)  
optimization of coupling

Significant gain obtained  
through AO and sensorless  
loop.  
Performance limited by AO  
system

**Coupling eff.  
measured  $\approx 10\%$   
SR  $\approx 11\%$**



# Conclusion

## Sensorless loop concept:

- A simple approach which goal is to simplify complex systems: use of single or no calibration source (improve transmission), ensure stability of system (reduce need for thermo-mechanical stabilisation), on the whole reduce costs.
- First demonstration: numerical analysis comforted by in lab experiment and first tests on sky
- Still a lot of job to be done :
  - Analysis of convergence wrt time averaging/nbr of actuator/modulation amplitude
  - Possibility to enhance strategy (choice of dithering basis, hierarchical approach ...)
  - Investigate fully automatic use of sensorless loop

## Applications:

- Long base interferometry, optical communication, ...