ANGULAR DIAMETERS AND EFFECTIVE TEMPERATURES OF 25 K GIANT STARS FROM THE CHARA ARRAY

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ABSTRACT

Using Georgia State University's Center for High Angular Resolution Astronomy Array interferometer, we measured angular diameters for 25 giant stars, six of which host exoplanets. The combination of these measurements and *Hipparcos* parallaxes produces physical linear radii for the sample. Except for two outliers, our values match angular diameters and physical radii estimated using photometric methods to within the associated errors with the advantage that our uncertainties are significantly lower. We also calculated the effective temperatures for the stars using the newly measured diameters. Our values do not match those derived from spectroscopic observations as well, perhaps due to the inherent properties of the methods used or because of a missing source of extinction in the stellar models that would affect the spectroscopic temperatures.

Key words: infrared: stars – planetary systems – stars: fundamental parameters – techniques: interferometric – techniques: spectroscopic

1. INTRODUCTION

Giant star radii have been measured in the past using various interferometers, including the Mark III (85 giants and supergiants; Mozurkewich et al. 2003), the Palomar Testbed Interferometer (69 giants and supergiants; van Belle et al. 1999), the Navy Prototype Optical Interferometer (50 giants and supergiants; Nordgren et al. 1999), and the Center for High Angular Resolution Astronomy (CHARA) Array (four Hyades giants; Boyajian et al. 2009). These measurements are valuable because these are the stars populating the coolest, most luminous part of the Hertzsprung–Russell (H–R) diagram (van Belle et al. 1999). What makes the sample of giant stars under consideration here particularly interesting is that they are potential exoplanet hosts, and planetary candidates have been discovered around six of the stars already.

Two important characteristics of a star are its mass and radius. For giant stars, the determination of these parameters is indirect and heavily model dependent. In practice, spectroscopic observations to measure the surface gravities ($\log g$), effective temperatures ($T_{\rm eff}$), and iron abundances ([Fe/H]) can be combined with a distance measurement to derive the stellar radius. Fitting evolutionary tracks to the position of the star in the H–R diagram then yields the mass. The reliability of these measurements depends both on the validity of the model atmospheres and the stellar evolution code. Unfortunately this is an uncertain process because the evolutionary tracks of stars with a wide range of masses all converge to near the same region of the H–R diagram as they evolve up the giant branch. In particular, the

mass estimates derived from evolutionary tracks depend critically on several parameters hidden in the tracks, such as the mixing length parameter and its assumed constancy for all stars, the unknown helium content in the core, and uncertainties about the nature of the convection zone. As a result, using different tracks can produce different masses, and in the absence of good calibrating objects no set of tracks can be claimed to provide the best results. On the other hand, if one can test and calibrate these evolutionary tracks by comparing the theoretically determined mass and radius to observed values, then one can have some faith in applying these tracks to stars for which direct measurements of these stellar parameters are not possible.

A star's mass is not only important for its evolution, but it should play an important role in the type of the planetary system a star will form. There are a number of Doppler surveys searching for planets around evolved giant stars with stellar masses of 1–2 M_{\odot} (e.g., Niedzielski et al. 2009; Döllinger et al. 2007; Setiawan et al. 2005; Sato et al. 2005). All are plagued by the same problem, in that they rely on evolutionary tracks to determine the stellar mass. Until these are calibrated both the mass of the host star and the planet are uncertain.

A more reliable means of calculating the stellar mass independent of evolutionary tracks and model atmospheres is using stellar oscillation observations, as the frequency of stellar oscillations is related to the mean density of the star. If one has an accurate stellar radius it is simple to compute a stellar mass from the oscillation frequencies that is model independent. Depending on the accuracy of the diameter measurements, the masses can be measured to an accuracy of $\sim 2\%$ (Teixeira et al. 2009) to $\sim 15\%$ (Hatzes & Zechmeister 2007). There is increasing evidence that most and possibly all giant stars show stellar oscillations (e.g., de Ridder et al. 2006; Frandsen, et al. 2002; Hatzes & Cochran 1994), which are due to p-mode oscillations where

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⁶ Some of the observations described here were completed while with the Center for High Angular Resolution Astronomy, Georgia State University, P.O. Box 3969, Atlanta, GA 30302-3969, USA.

 Table 1

 Observed and Spectroscopic Properties of the K Giants

Target HD	V mag	K mag	Spec Type	π (mas)	<i>T</i> _{eff} ±70 K	log g ±0.2	[Fe/H] ±0.5 dex	θ _{estimate} (mas)	$R_{ m estimate} \ (R_{\odot})$	$M_{ m estimate}$ (M_{\odot})
32518	6.41	3.91 ± 0.04^{a}	K1 III	8.29 ± 0.58	4580	2.0	-0.15	0.84 ± 0.05	10.9 ± 1.0	1.1 ± 0.2
60294	5.92	3.55 ± 0.22^{a}	K2 III	12.24 ± 0.39	4520	2.4	+0.02	0.97 ± 0.31	8.5 ± 2.7	1.2 ± 0.1
73108	4.60	1.92 ± 0.07^{b}	K1 III	12.74 ± 0.26	4415	1.8	-0.25	2.17 ± 0.22	18.3 ± 1.9	1.2 ± 0.2
102328	5.29	2.55 ± 0.06^{b}	K3 III	15.13 ± 0.30	4250	1.9	+0.09	1.64 ± 0.14	11.6 ± 1.0	1.1 ± 0.1
103605	5.84	3.10 ± 0.30^{a}	K1 III	10.54 ± 0.37	4740	2.8	-0.07	1.27 ± 0.54	12.9 ± 5.5	1.1 ± 0.2
106574	5.71	2.94 ± 0.08^{b}	K2 III	7.00 ± 0.28	4570	2.2	-0.31	1.38 ± 0.16	21.1 ± 2.6	1.6 ± 0.2
113049	6.00	3.66 ± 0.31^{a}	K0 III	6.02 ± 0.37	4740	2.2	-0.18	0.92 ± 0.41	16.4 ± 7.3	2.2 ± 0.3
118904	5.51	2.69 ± 0.07^{b}	K2 III	7.93 ± 0.24	4500	2.2	-0.18	1.55 ± 0.16	21.1 ± 2.2	1.4 ± 0.2
136726	5.01	1.92 ± 0.05^{b}	K4 III	8.19 ± 0.19	4340	1.6	+0.04	2.33 ± 0.17	30.5 ± 2.4	2.0 ± 0.2
137443	5.79	2.74 ± 0.06^{b}	K4 III	8.86 ± 0.22	4435	2.6	-0.03	1.58 ± 0.14	19.2 ± 1.7	1.4 ± 0.2
138265	5.88	2.38 ± 0.04^{b}	K5 III	5.11 ± 0.31	4200	2.4	-0.07	2.02 ± 0.12	42.5 ± 3.6	1.5 ± 0.2
139357	5.97	3.41 ± 0.32^{a}	K4 III	8.47 ± 0.30	4700	2.9	-0.13	1.07 ± 0.49	13.6 ± 6.2	1.3 ± 0.2
150010	6.28	3.18 ± 0.38^{a}	K2 III	6.95 ± 0.43	4540	2.8	-0.02	1.31 ± 0.71	20.2 ± 11.1	1.4 ± 0.3
152812	6.00	2.83 ± 0.09^{b}	K2 III	4.97 ± 0.45	4220	1.4	-0.42	1.55 ± 0.20	33.5 ± 5.3	1.1 ± 0.1
157681	5.67	2.19 ± 0.05^{b}	K5 III	5.23 ± 0.27	4400	1.6	-0.23	2.20 ± 0.16	45.2 ± 4.1	1.7 ± 0.3
160290	5.36	2.67 ± 0.07^{b}	K1 III	9.23 ± 0.21	4750	2.7	-0.17	1.54 ± 0.16	17.9 ± 1.9	2.0 ± 0.3
167042	5.98	3.55 ± 0.24^{a}	K1 III	19.91 ± 0.26	4820	2.9	-0.08	0.98 ± 0.33	5.3 ± 1.8	1.2 ± 0.1
170693	4.83	1.95 ± 0.05^{b}	K1.5 III	10.36 ± 0.20	4200	1.0	-0.46	2.21 ± 0.16	22.9 ± 1.7	1.0 ± 0.1
175823	6.22	3.57 ± 0.32^{a}	K5 III	5.63 ± 0.28	4500	2.1	-0.12	1.01 ± 0.46	19.2 ± 8.7	1.7 ± 0.2
176408	5.66	3.00 ± 0.27^{a}	K1 III	11.81 ± 0.27	4500	2.3	-0.06	1.31 ± 0.50	12.0 ± 4.6	1.1 ± 0.2
186815	6.28	4.32 ± 0.25^{a}	K2 III	12.86 ± 0.39	4900	2.5	-0.32	0.63 ± 0.23	5.3 ± 1.9	1.2 ± 0.1
192781	5.79	2.33 ± 0.07^{b}	K5 III	5.62 ± 0.23	4210	2.3	-0.08	2.05 ± 0.21	39.3 ± 4.3	1.4 ± 0.2
195820	6.18	3.90 ± 0.22^{a}	K0 III	8.68 ± 0.29	4710	2.4	-0.16	0.81 ± 0.25	10.1 ± 3.2	1.0 ± 0.2
200205	5.51	2.25 ± 0.06^{b}	K4 III	5.30 ± 0.24	4210	1.6	-0.28	2.06 ± 0.18	41.7 ± 4.1	1.3 ± 0.2
214868	4.48	1.41 ± 0.07^{b}	K2 III	9.80 ± 0.26	4440	2.1	-0.18	2.93 ± 0.30	32.1 ± 3.4	1.8 ± 0.2

Notes. V magnitudes are from Mermilliod (1991) and spectral types are from the SIMBAD Astronomical Database; parallaxes (π) are from van Leeuwen (2007a, 2007b); $T_{\rm eff}$, log g, [Fe/H] are from Döllinger (2008); $\theta_{\rm estimate}$ and $R_{\rm estimate}$ were determined photometrically, and $M_{\rm estimate}$ is from the PARAM Stellar Model (da Silva et al. 2006).

pressure is the restoring force. Thus, giant stars are an ideal class of objects for deriving fundamental stellar parameters. They are abundant, they have large angular diameters suitable for interferometric measurements, and they exhibit stellar oscillations with radial velocity amplitudes of a few to several tens of m s^{-1} , which are easily measurable by state-of-the-art techniques. The observed oscillation frequencies constrain the internal structure of the star (Bedding et al. 2006) and interferometry measures the star's size, and the combination leads to the mass of the star. Once stellar isochrones have been refined and calibrated for these evolved stars, they can be used to determine the masses of all planet-hosting giant stars. Because collecting data on the oscillation frequencies requires considerable telescope resources and can only be done for relatively few stars, we first present our results on interferometric measurements on a larger sample of giant stars.

The advantage interferometry provides is the ability to directly measure stellar angular diameters. Once the angular diameters are known for these giant stars, physical radii and effective temperatures can be calculated when combined with other parameters, such as the parallax, bolometric flux, interstellar absorption, and bolometric corrections (BCs). The radii and effective temperatures are important values that characterize the parent star as well as the environment in which the exoplanet resides for those stars hosting planets. Section 2 describes the spectroscopic measurements of $T_{\rm eff}$ and log g for the sample, Section 3 discusses the interferometric observations, Section 4 explains how the angular diameters, linear radii, and $T_{\rm eff}$ were

determined, and Section 5 explores the physical implications of the interferometric observations.

2. SPECTROSCOPIC OBSERVATIONS

Our sample of K giant stars were obtained from the planet search survey of Döllinger et al. (2007). As part of this program the T_{eff} and $\log g$ were measured, which allowed us to estimate the stellar radii and masses. Table 1 lists the 25 stars observed here, and planets have already been found orbiting HD 73108 (Döllinger et al. 2007), HD 139357 and HD 170693 (Döllinger et al. 2009a), HD 32518 and HD 136726 (Döllinger et al. 2009b), and HD 167042 (Johnson et al. 2008; Sato et al. 2008; M. P. Döllinger et al. 2010a, in preparation). Three additional stars show long-period variations in their radial velocity measurements: HD 106574, HD 157681, and HD 200205 (M. P. Döllinger et al. 2010b, in preparation). The targets chosen for our observing list are bright (V < 6.5) giant stars that showed significant short-term variability indicative of stellar pulsations, which made them excellent candidates for both stellar oscillation observations and interferometric measurements.

The spectroscopic observations were carried out using the Coudé Échelle spectrograph of the 2 m Alfred Jensch telescope of the Thüringer Landessternwarte Tautenburg. The spectrograph has a resolving power of $\Delta\lambda/\lambda=67,000$ and the wavelength range used was 4700-7400 Å. Standard IRAF routines were used for subtracting the bias offset, flat-fielding,

^a 2MASS All-Sky Catalog of Point Sources (Cutri et al. 2003).

^b Two-Micron Sky Survey (Neugebauer & Leighton 1969).

 Table 2

 Observing Log and Calibrator Stars' Basic Parameters

		Observing Log			Calibrator Information				
Target HD	Calibrator HD	Baseline ^a (max. length)	Date (UT)	Obs	$T_{\rm eff}^{\rm b}$ (K)	$\log g^{\rm b}$ $({\rm cm \ s}^{-2})$	$\theta_{\mathrm{LD}}^{\mathrm{c}}$ (mas)		
32518	31675	S1-E1 (331 m)	2007 Nov 14	9	6310	4.39	0.401 ± 0.015		
60294	63332	S1-E1 (331 m)	2009 Apr 23	5	6310	4.19	0.431 ± 0.014		
	69548		•	5	6761	4.31	0.402 ± 0.018		
73108	69548	E2-W2 (156 m)	2008 May 9	5	6761	4.31	0.402 ± 0.018		
102328	98673	S1-E1 (331 m)	2009 Apr 24	3	8128	4.21	0.220 ± 0.010		
	108954		_	2	6026	4.34	0.452 ± 0.021		
103605	108954	S1-E1 (331 m)	2009 Apr 22	4	6026	4.34	0.452 ± 0.021		
	98673		2009 Apr 24	3	8128	4.21	0.220 ± 0.010		
	108954		•	3	6026	4.34	0.452 ± 0.021		
106574	107193	E2-W2 (156 m)	2008 Jun 29	6	8710	3.93	0.315 ± 0.030		
113049	107193	S1-E1 (331 m)	2009 Apr 23	8	8710	3.93	0.315 ± 0.030		
	124063			5	7740	4.29	0.232 ± 0.010		
118904	124063	E2-W2 (156 m)	2008 Jun 29	6	7740	4.29	0.232 ± 0.010		
136726	145454	E2-W2 (156 m)	2008 May 9	6	9772	4.13	0.268 ± 0.015		
137443	145454	E2-W2 (156 m)	2008 May 9	6	9772	4.13	0.268 ± 0.015		
138265	145454	E2-W2 (156 m)	2008 May 9	4	9772	4.13	0.268 ± 0.015		
			2008 May 11	3					
139357	132254	S1-E1 (331 m)	2007 Sep 14	4	6310	4.27	0.521 ± 0.015		
			2007 Sep 15	3					
150010	145454	E2-W2 (156 m)	2008 Jun 29	6	9772	4.13	0.268 ± 0.015		
	149681	S1-E1 (331 m)	2008 Jul 17	4	7586	4.23	0.368 ± 0.012		
152812	149303	S1-E1 (331 m)	2009 Apr 20	4	8511	4.10	0.288 ± 0.011		
	151044			5	6166	4.38	0.380 ± 0.008		
157681	158460	S1-E1 (331 m)	2007 Sep 14	5	9000	4.19	0.268 ± 0.016		
160290	158414	S1-E1 (331 m)	2009 Apr 24	6	8000	4.24	0.295 ± 0.012		
	161693			4	9000	4.19	0.258 ± 0.015		
167042	161693	S1-E1 (331 m)	2007 Sep 15	8	9000	4.19	0.258 ± 0.015		
170693	172569	W1-S2 (249 m)	2007 Sep 3	4	7413	3.98	0.309 ± 0.013		
175823	172728	S1-E1 (331 m)	2009 Apr 23	4	9790	4.14	0.236 ± 0.020		
	178207			6	9790	4.14	0.271 ± 0.015		
176408	172728	S1-E1 (331 m)	2009 Apr 23	4	9790	4.14	0.236 ± 0.020		
	178207			6	9790	4.14	0.271 ± 0.015		
186815	186760	S1-E1 (331 m)	2009 Apr 24	7	6026	3.90	0.432 ± 0.019		
	188793			9	8800	4.21	0.226 ± 0.016		
192781	186760	S1-E1 (331 m)	2009 Apr 24	7	6026	3.90	0.432 ± 0.019		
	188793			9	8800	4.21	0.226 ± 0.016		
195820	184960	S1-E1 (331 m)	2007 Nov 14	4	6457	4.33	0.492 ± 0.019		
200205	197950	W1-S2 (249 m)	2007 Sep 3	8	7762	4.30	0.349 ± 0.014		
214868	211211	E2-W2 (156 m)	2008 Jun 29	4	9333	4.17	0.249 ± 0.015		
		S1-E1 (331 m)	2008 Jul 1	3					

Notes.

subtracting the scattered light, extracting the spectra, and for the wavelength calibration. 7

In order to determine the stellar parameters from the spectra, a grid of model atmospheres from Gustafsson et al. (1975) was used in which a plane-parallel atmosphere in local thermodynamic equilibrium was assumed. We selected 144 unblended Fe I

and eight Fe II lines in the wavelength range 5806 and 6858 Å using the line list of Pasquini et al. (2004). The iron abundance [Fe/H] was determined by assuming that Fe I lines of different equivalent widths have to give the same relative abundance of iron. For the effective temperature, an excitation equilibrium of Fe I and Fe II for lines of different excitation potentials was used, and the surface gravity was determined from the ionization balance of Fe I to Fe II lines (Döllinger 2008). The resulting [Fe/H], $T_{\rm eff}$, and log g values are listed in Table 1.

^a The three arms of the array are denoted by their cardinal directions: "S" is south, "E" is east, and "W" is west. Each arm bears two telescopes, numbered "1" for the telescope farthest from the beam combining laboratory and "2" for the telescope closer to the lab. ^b All $T_{\rm eff}$ and log g values are from Allende Prieto & Lambert (1999) except for HD 124063, HD 158414, HD 158460, HD 161693, HD 172728, HD 178207, and HD 188793, which are from Cox (2000) and were based on their spectral types as listed in the SIMBAD Astronomical Database.

^c In calculating θ_{LD} as described in Section 3, the *UBV* values were from Mermilliod (1991) except for HD 149303 (ESA 1997), and HD 151044 and HD 184960 (Morel & Magnenat 1978); all *RI* values were from Monet et al. (2003) except for HD 151044 and HD 184960 (Morel & Magnenat 1978); and all *JHK* values were from Cutri et al. (2003).

⁷ IRAF is distributed by the National Optical Astronomy Observatories, which are operated by the Association of Universities for Research in Astronomy, Inc., under cooperative agreement with the National Science Foundation.

Table 3
K Giants' Calibrated Visibilities

Table 3 (Continued)

1958 1967	Target HD	Calibrator HD	MJD	<i>B</i> (m)	Θ (deg)	V_c	σV_c	Target HD	Calibrator HD	MJD	<i>B</i> (m)	Θ (deg)	V_c	σV_c
1481-20 1481			54418 238			0.755	0.067	пр	пр	54505 207			0.425	0.045
14 14 15 15 16 16 16 16 16 16	32316	31073												
14 14 15 15 16 16 16 16 16 16														
14 15 15 15 15 15 15 15						0.843								0.062
1			54418.261	241.66	206.9	0.751	0.061					206.5		0.053
1481 1481								137443	145454		155.65	219.1	0.673	0.082
6418-286 5418-286 5418-286 5418-286 5418-286 5419-416													0.631	0.083
69/2014 69/3124 69/3441 (3) 89.9 9.9 0.944 0.045														
14 14 15 15 15 15 15 15	60204	62222												
1840 1841 1842 1848 1842 1844 1845 1845 1854 1855 1858	00294	03332												
1494-101 1494-101								129265	145454					
								136203	143434					
14 14 15 15 15 15 15 15														
14 14 15 15 15 15 15 15		69548	54944.160		91.0	0.526								0.070
744 (20) 318.44 100.8 0.505 0.502 5.944.00 155.16 224.4 0.489 0.050 73108 65948 5495.216 155.59 254.7 0.411 0.051 139357 132254 54357.163 320.75 102.8 0.400 0.045 73108 6595.226 155.85 254.7 0.411 0.043 0.033 54357.161 319.12 101.0 0.040 0.043 4595.227 155.77 268.4 0.450 0.057 268.2 0.435 0.057 34358.157 319.17 10.03 0.400 0.000 102228 9867 5495.257 135.77 268.4 0.480 0.011 5495.261 319.17 0.015 0.000 34358.157 310.0 0.015 0.000 34358.163 319.17 0.057 0.029 0.002 34366.323 310.0 0.029 0.004 0.002 34366.323 0.003 0.003 0.002 34366.323 0.003 0.002 34366.323			54944.168	319.64	92.9	0.448	0.057			54597.467	155.50	246.2	0.559	0.079
73108 69548 54945208 317.93 102.7 0.455 0.053 139357 132254 54357.163 320.14 104.2 0.040 0.007 73108 69548 54395.226 155.88 28.0 0.446 0.034 - 54357.161 319.6 105.6 0.467 0.030 4595.244 155.80 261.1 0.406 0.0037 - 54358.157 319.21 107.0 0.401 0.006 102328 98673 54395.257 3146.3 225.0 0.088 0.009 15001 145455 54358.157 31.03 0.415 0.049 10232 98673 5495.259 314.03 228.0 0.088 0.009 150010 145455 5466.318 15.39 26.1 0.035 0.122 10232 91.0 0.010 0.012 - 5466.338 15.30 26.1 0.035 0.122 10345 91.0 0.437 0.027 - 5466.338 15.54										54597.477	155.33	249.3	0.500	0.061
73108 69548 54595_216 155.95 2547 0.411 0.051														0.061
1498 54995.226 155.88 258.0 0.446 0.034 54357.161 319.02 105.0 0.047 0.003 1493 224 155.80 264.1 0.460 0.037 54358.151 319.24 103.9 0.040 0.030 102328 98673 5495.239 314.63 282.0 0.080 0.011 145454 5405.181 319.27 105.7 0.429 0.040 102328 98673 54945.239 314.63 248.9 0.00 0.012 5405.6318 154.04 22.10 0.033 0.11 10805 54945.239 314.63 248.9 0.00 0.012 54646.335 154.84 22.10 0.83 0.11 10305 9495 54943.337 314.63 243.9 0.00 0.02 54646.335 154.85 23.1 0.83 0.11 10305 9495.239 314.63 124.9 0.02 0.02 5464.634 155.07 232.1 0.83 0.01	52400	60.7.10						139357	132254					
102328	/3108	69548												
1808 1808 1808 1808 1808 1808 1808 1808 1808 1809														
102228														
102328 98673 54945.299 314.63 248.9 0.086 0.011 5.0100 145454 54646.318 151.90 10.27 0.0.7 0.4.29 0.012 0.012 5.0102 5.0														
108954 54945.252 316.18 252.0 0.088 0.009 150010 145454 54646.318 154.39 226.3 0.785 0.125 108954 54945.293 314.63 248.9 0.100 0.012 54646.335 154.85 231.9 0.832 0.085 108954 54945.294 317.31 254.8 0.095 0.012 54646.335 155.07 235.1 0.835 0.113 103605 108954 54943.375 317.53 99.1 0.437 0.027 54646.335 155.07 235.1 0.835 0.113 54943.388 317.18 100.6 0.442 0.032 54646.336 155.07 235.1 0.822 0.083 54943.384 316.37 103.5 0.409 0.029 54664.305 54664.302 273.81 117.3 0.822 0.083 54943.394 316.37 103.5 0.409 0.029 54664.303 54664.403 270.01 120.2 0.589 0.086 54945.280 316.51 256.9 0.446 0.062 152812 149303 54941.409 327.27 256.0 0.152 0.014 108954 54945.280 316.51 256.9 0.446 0.062 152812 149303 54941.409 327.27 256.0 0.152 0.014 108954 54945.280 316.51 256.9 0.446 0.062 152812 149303 54941.409 327.27 256.0 0.152 0.014 108954 54945.280 316.51 256.9 0.449 0.069 0.099	102328	98673												
10895								150010	145454					
108954 54945.229 314.63 248.9 0.100 0.1012 54646.335 154.85 231.9 0.823 0.825			54945.290	319.04	261.0	0.073	0.011							
108954		108954	54945.239	314.63	248.9	0.100	0.012							0.085
1895 1895 1894 1892 1894 1892 1894 1892 1894										54646.345	155.07	235.1	0.835	0.113
\$4943.388 316.77 102.2	103605	108954												0.125
1895 54943,394 316.37 103.5 0.409 0.029 54664.433 272.04 120.2 0.589 0.096 54945,242 312.54 248.0 0.445 0.048 54664.433 270.21 123.0 0.640 0.080 54945,2580 316.51 256.9 0.446 0.062 152812 149303 54941.490 327.27 256.0 0.152 0.014 108954 54945,267 315.40 253.8 0.465 0.069 0.054 54941.490 327.27 256.0 0.152 0.014 54945,280 316.51 256.9 0.489 0.054 54941.697 327.94 259.9 0.164 0.015 54945,280 316.51 256.9 0.489 0.054 54941.507 327.94 259.9 0.154 0.010 54945,280 316.51 256.9 0.489 0.054 54941.507 327.94 259.9 0.154 0.010 54945,280 317.37 260.2 0.449 0.044 54941.516 328.18 261.9 0.148 0.015 54646,187 155.91 241.7 0.699 0.099 15104 54941.481 326.75 253.8 0.158 0.017 54646,196 155.99 244.8 0.698 0.131 54941.490 327.27 256.0 0.154 0.016 54646,214 156.11 250.8 0.680 0.086 54941.90 327.63 257.9 0.168 0.015 54646,223 156.14 253.9 0.732 0.085 54941.507 327.94 259.9 0.157 0.011 54646,223 156.14 253.9 0.732 0.085 54941.507 327.94 259.9 0.157 0.011 54646,223 156.14 253.9 0.050 0.086 54941.516 328.18 261.9 0.154 0.016 54944,370 272.37 267.4 0.630 0.051 54954.513 320.64 104.8 0.057 0.005 54944,370 272.37 267.4 0.630 0.051 54954.513 320.64 104.8 0.057 0.005 54944,370 272.37 267.4 0.630 0.051 54954.533 259.5 319.8 309.4 0.006 0.004 54944,370 272.17 267.4 0.587 0.009 0.052 0.007 54954.536 292.52 223.8 0.250 0.003 54944,411 271.80 99.0 0.633 0.076 0.052 0.054 54945.356 292.52 223.8 0.250 0.035 54944,411 271.80 99.0 0.633 0.076 0.052 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.054 0.05														
\$\begin{small} \qqq \q									149681					
10895		98673												
108954 54945.280 316.51 256.9 0.446 0.062 152812 149303 54941.490 327.27 256.0 0.152 0.014 108954		70073												
108954								152812	149303					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		108954						102012	1.7505					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			54945.280	316.51	256.9	0.489	0.054							0.010
54646.196										54941.516	328.18	261.9	0.148	0.015
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	106574	107193							151044	54941.481			0.158	0.017
113049 107193 54646.234 156.11 250.8 0.680 0.086 54941.507 327.94 259.9 0.157 0.011 113049 107193 54944.362 272.32 265.1 0.655 0.059 54941.516 328.18 261.9 0.154 0.016 54944.370 272.47 267.4 0.630 0.051 54357.211 321.92 99.9 0.056 0.004 54944.386 272.53 269.5 0.692 0.070 54357.211 321.92 99.9 0.056 0.004 54944.386 272.53 269.5 0.692 0.070 54357.211 321.92 321.36 102.3 0.055 0.005 54944.394 272.57 267.4 0.630 0.051 54357.231 320.64 104.8 0.057 0.005 54944.394 272.57 94.4 0.687 0.049 0.052 54357.251 318.83 109.4 0.060 0.010 54944.394 272.37 94.4 0.587 0.049 160290 158414 54945.330 279.04 219.2 0.267 0.020 54944.411 271.80 99.0 0.633 0.076 54945.366 292.52 223.8 0.250 0.037 54944.395 272.32 265.1 0.611 0.059 54945.366 292.52 223.8 0.250 0.037 54944.396 272.32 265.1 0.611 0.059 54945.366 292.52 223.8 0.250 0.037 54944.370 272.47 267.4 0.542 0.035 54945.366 292.52 223.8 0.225 0.026 54944.378 272.53 269.5 0.602 0.048 161693 54945.366 292.52 223.8 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 54944.419 271.38 101.3 0.656 0.058 161693 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074														
113049 107193 54646.234 156.18 257.5 0.701 0.081 157681 158460 54941.516 328.18 261.9 0.154 0.016 0.004 0.004 0.005 0.004 0.005 0.004 0.005 0.004 0.005														
113049 107193														
113049 107193 54944.362 272.32 265.1 0.655 0.059 54357.221 321.36 102.3 0.056 0.005 54944.370 272.47 267.4 0.630 0.051 54944.378 272.53 269.5 0.692 0.070 54357.241 319.83 107.1 0.060 0.004 54944.378 272.53 269.5 0.692 0.070 54357.251 318.83 109.4 0.060 0.004 54944.394 272.37 94.4 0.587 0.049 160290 158414 54945.330 279.04 219.2 0.267 0.020 54944.403 272.12 96.8 0.605 0.049 54944.411 271.80 99.0 0.633 0.076 54944.411 271.80 99.0 0.633 0.076 54944.411 271.80 99.0 0.633 0.076 54944.411 271.80 99.0 0.633 0.076 54944.411 271.80 99.0 0.633 0.076 54944.411 271.80 99.0 0.633 0.076 54944.370 272.47 267.4 0.542 0.055 54944.370 272.47 267.4 0.542 0.055 54944.370 272.47 267.4 0.542 0.055 54944.378 272.53 269.5 0.602 0.048 161693 54945.336 292.52 223.8 0.250 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 118904 124063 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 118904 124063 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 118904 124063 54944.411 271.80 99.0 0.581 0.070 54945.366 292.52 223.8 0.225 0.026 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.356 292.52 223.8 0.225 0.026 118904 124063 54646.261 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.245 319.96 103.1 0.571 0.036								157601	159460					
54944.370 272.47 267.4 0.630 0.051 54357.231 320.64 104.8 0.057 0.005 54944.378 272.53 269.5 0.692 0.070 54357.241 319.83 107.1 0.060 0.004 54944.386 272.50 91.9 0.670 0.052 54357.251 318.83 109.4 0.060 0.010 54944.394 272.37 94.4 0.587 0.049 160290 158414 54945.330 279.04 219.2 0.267 0.020 54944.410 271.38 101.3 0.696 0.071 54945.339 283.87 220.7 0.280 0.030 124063 54944.362 272.32 265.1 0.611 0.059 54945.366 292.52 223.8 0.250 0.037 124063 54944.378 272.53 269.5 0.602 0.048 161693 54945.366 292.52 223.8 0.225 0.025 54944.411 271.80 99.0 0.581	113049	107193						13/061	136400					
189044.378 272.53 269.5 0.692 0.070 54357.241 319.83 107.1 0.060 0.004 54944.386 272.50 91.9 0.670 0.052 54357.251 318.83 109.4 0.060 0.010 54944.394 272.37 94.4 0.587 0.049 160290 158414 54945.330 279.04 219.2 0.267 0.020 54944.403 272.12 96.8 0.605 0.049 54945.330 279.04 219.2 0.267 0.020 54944.411 271.80 99.0 0.633 0.076 54945.348 288.23 222.2 0.247 0.030 54944.370 272.47 267.4 0.542 0.035 54945.366 292.52 223.8 0.250 0.022 54944.378 272.53 269.5 0.602 0.048 161693 54945.375 300.60 227.4 0.172 0.022 54944.411 271.80 99.0 0.581 0.070 54945.376 292.52 223.8 0.228 0.027 54945.376 54944.411														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			54944.378	272.53	269.5	0.692	0.070							0.004
54944.403 272.12 96.8 0.605 0.049 54945.339 283.87 220.7 0.280 0.030 54944.411 271.80 99.0 0.633 0.076 54945.338 288.23 222.2 0.247 0.030 54944.419 271.38 101.3 0.696 0.071 54945.356 292.52 223.8 0.250 0.037 124063 54944.362 272.32 265.1 0.611 0.059 54945.356 292.52 223.8 0.250 0.037 54944.370 272.47 267.4 0.542 0.035 54945.356 296.96 225.7 0.217 0.042 54944.411 271.80 99.0 0.581 0.070 54945.356 292.52 223.8 0.228 0.027 54944.419 271.38 101.3 0.656 0.058 54945.356 292.52 223.8 0.228 0.027 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.356 292.52 223.8 0.227.4 0.167 0.017 54646.268			54944.386	272.50	91.9	0.670	0.052					109.4	0.060	0.010
124063 54944.411 271.80 99.0 0.633 0.076 54945.348 288.23 222.2 0.247 0.030 124063 54944.362 272.32 265.1 0.611 0.059 54945.366 296.96 225.7 0.217 0.042 54944.370 272.47 267.4 0.542 0.035 54945.375 300.60 227.4 0.172 0.022 54944.378 272.53 269.5 0.602 0.048 161693 54945.348 288.23 222.2 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 296.96 225.7 0.172 0.022 54944.419 271.38 101.3 0.656 0.058 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54945.375 54666.260 155.89 247.3			54944.394	272.37	94.4	0.587		160290	158414	54945.330	279.04	219.2	0.267	0.020
124063 54944.419 271.38 101.3 0.696 0.071 54945.356 292.52 223.8 0.250 0.037 124063 54944.362 272.32 265.1 0.611 0.059 54945.366 296.96 225.7 0.217 0.042 54944.370 272.47 267.4 0.542 0.035 54945.375 300.60 227.4 0.172 0.022 54944.378 272.53 269.5 0.602 0.048 161693 54945.348 288.23 222.2 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 118904 124063 54646.261 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037										54945.339	283.87	220.7	0.280	0.030
124063 54944.362 272.32 265.1 0.611 0.059 54945.366 296.96 225.7 0.217 0.042 54944.370 272.47 267.4 0.542 0.035 54945.375 300.60 227.4 0.172 0.022 54944.378 272.53 269.5 0.602 0.048 161693 54945.348 288.23 222.2 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.366 296.96 225.7 0.183 0.027 54944.419 271.38 101.3 0.656 0.058 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088														
118904 124063 54944.370 272.47 267.4 0.542 0.035 54945.375 300.60 227.4 0.172 0.022 118904 124063 54944.378 272.53 269.5 0.602 0.048 161693 54945.348 288.23 222.2 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.356 292.52 223.8 0.228 0.027 54944.419 271.38 101.3 0.656 0.058 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 <		124062												
118904 124063 54944.378 272.53 269.5 0.602 0.048 161693 54945.348 288.23 222.2 0.225 0.026 54944.411 271.80 99.0 0.581 0.070 54945.356 292.52 223.8 0.228 0.027 54944.419 271.38 101.3 0.656 0.058 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.34 101.7 0.524 0.030 54646.288 156.05		124063												
118904 124063 54944.411 271.80 99.0 0.581 0.070 54945.356 292.52 223.8 0.228 0.027 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.366 296.96 225.7 0.183 0.021 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036									161602					
118904 124063 54944.419 271.38 101.3 0.656 0.058 54945.366 296.96 225.7 0.183 0.021 118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036									101093					
118904 124063 54646.251 155.81 244.4 0.574 0.074 54945.375 300.60 227.4 0.167 0.017 54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036														
54646.260 155.89 247.3 0.567 0.069 167042 161693 54358.232 321.20 97.5 0.584 0.037 54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036	118904	124063												
54646.268 155.95 250.1 0.589 0.060 54358.238 320.96 99.0 0.551 0.036 54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036								167042	161693					0.037
54646.278 156.01 253.3 0.512 0.064 54358.243 320.68 100.3 0.507 0.036 54646.288 156.05 256.6 0.583 0.070 54358.249 320.34 101.7 0.524 0.030 54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036			54646.268	155.95	250.1	0.589	0.060							0.036
54646.297 156.08 259.6 0.562 0.088 54358.255 319.96 103.1 0.571 0.036										54358.243	320.68	100.3	0.507	0.036
· · · · · · · · · · · · · · · · · · ·										54358.249		101.7	0.524	0.030
- 13D//D - 140404 - 04090 794 - 14/07 - 189 4 - 10407 - 1000 - 10	126726	145454												0.036
34338.201 319.33 104.3 0.012 0.037	130/26	145454	54595.294	14/.5/	189.4	0.442	0.055			54358.261	319.53	104.5	0.612	0.037

Table 3 (Continued)

Table 3 (Continued)

			inueu)			
Target HD	Calibrator HD	MJD	<i>B</i> (m)	Θ (dag)	V_c	σV_c
	ПБ	54259 267	319.05	(deg)	0.501	0.041
		54358.267 54358.273	319.05	105.9 107.4	0.591 0.627	0.041 0.050
170693	172569	54346.303	187.40	183.8	0.027	0.030
170075	172307	54346.311	183.87	186.6	0.343	0.042
		54346.321	179.32	190.2	0.358	0.037
		54346.332	174.70	193.9	0.457	0.042
175823	172728	54944.471	297.24	232.9	0.499	0.044
		54944.482	300.30	235.4	0.480	0.064
		54944.493	303.23	238.1	0.553	0.065
		54944.505	305.73	240.8	0.533	0.056
	178207	54944.442	287.69	226.5	0.633	0.071
		54944.454	291.73	229.0	0.667	0.053
		54944.471	297.24	232.9	0.590	0.052
		54944.482	300.30	235.4	0.576	0.082
		54944.493 54944.505	303.23	238.1 240.8	0.569	0.060
176408	172728	54944.473	305.73 296.67	232.9	0.580 0.409	0.045 0.043
170400	172720	54944.484	299.83	235.5	0.409	0.043
		54944.496	302.66	238.1	0.436	0.059
		54944.507	305.17	240.8	0.416	0.046
	178207	54944.445	287.23	226.5	0.585	0.060
		54944.456	291.14	228.9	0.587	0.055
		54944.473	296.67	232.9	0.501	0.053
		54944.484	299.83	235.5	0.462	0.058
		54944.496	302.66	238.1	0.452	0.057
		54944.507	305.17	240.8	0.465	0.039
186815	186760	54945.396	248.69	209.6	0.792	0.082
		54945.408	256.16	212.2	0.891	0.083
		54945.419	262.58	214.5	0.732	0.056
		54945.429 54945.440	268.32 273.75	216.8 219.1	0.777 0.764	0.069 0.072
		54945.484	292.08	228.8	0.704	0.072
		54945.495	295.81	231.3	0.740	0.058
	188793	54945.396	248.69	209.6	0.749	0.098
		54945.408	256.16	212.2	0.929	0.111
		54945.419	262.58	214.5	0.760	0.082
		54945.429	268.32	216.8	0.699	0.075
		54945.440	273.75	219.1	0.742	0.069
		54945.461	283.52	223.8	0.783	0.058
		54945.473	287.96	226.3	0.778	0.040
		54945.484	292.08	228.8	0.761	0.044
102701	196760	54945.495	295.81	231.3	0.726	0.057
192781	186760	54945.400 54945.411	231.04 238.31	202.6 205.2	0.225 0.202	0.027 0.017
		54945.422	245.12	203.2	0.202	0.017
		54945.432	251.29	210.4	0.174	0.012
		54945.443	257.29	212.9	0.140	0.012
		54945.487	277.78	223.2	0.078	0.005
		54945.498	282.14	225.9	0.062	0.004
	188793	54945.400	231.04	202.6	0.220	0.032
		54945.411	238.31	205.2	0.214	0.024
		54945.422	245.12	207.9	0.173	0.018
		54945.432	251.29	210.4	0.154	0.016
		54945.443	257.29	212.9	0.143	0.012
		54945.464	268.07	218.0	0.109	0.010
		54945.476	273.15	220.6	0.091	0.006
		54945.487	277.78	223.2	0.074	0.004
195820	184960	54945.498 54418 160	282.14	225.9	0.062	0.004
193020	104900	54418.169 54418.184	323.56 322.84	98.4 102.0	0.626 0.703	0.070 0.076
		54418.194	322.84	102.0	0.703	0.076
		54418.203	321.50	104.2	0.610	0.051
200205	197950	54346.350	214.19	161.4	0.327	0.032
		54346.358	211.24	163.5	0.309	0.039

Target	Calibrator	MJD	B	Θ	V_c	σV_c
HD	HD		(m)	(deg)		
		54346.365	208.36	165.4	0.267	0.030
		54346.372	205.28	167.4	0.302	0.039
		54346.378	202.26	169.3	0.338	0.033
		54346.385	199.22	171.2	0.242	0.021
		54346.392	195.69	173.3	0.267	0.035
		54346.406	188.87	177.4	0.318	0.031
214868	211211	54646.402	138.11	183.1	0.361	0.072
		54646.413	141.40	185.6	0.352	0.042
		54646.423	144.26	188.0	0.326	0.054
		54646.433	146.89	190.5	0.304	0.058
		54648.457	322.39	239.2	0.073	0.012
		54648.469	324.32	241.8	0.064	0.005
		54648.479	325.51	243.8	0.079	0.007

Note. The projected baseline position angle (Θ) is calculated to be east of north.

3. INTERFEROMETRIC OBSERVATIONS

Interferometric observations were obtained using the CHARA Array, a six element optical-infrared interferometer located on Mount Wilson, California (ten Brummelaar et al. 2005). All observations used the pupil-plane "CHARA Classic" beam combiner in the K' band at 2.15 μ m, while visible wavelengths (470–800 nm) were used for tracking and tip/tilt corrections. The observing procedure and data reduction process employed here are described in McAlister et al. (2005).

We interleaved calibrator and target star observations so that every target was flanked by calibrator observations made as close in time as possible, which allowed us to convert instrumental target and calibrator visibilities to calibrated visibilities for the target. Reliable calibrators were chosen to be single stars with expected visibility amplitudes >85% so they were nearly unresolved on the baselines used, which meant uncertainties in the calibrator's diameter did not affect the target's diameter calculation as much as if the calibrator star had a significant angular size. In a few cases, a calibrator had a stellar companion but at such a distance that light from the secondary star would not contaminate our interferometric measurements and the calibrator could therefore be treated as a single star.

To check for possible unseen close companions that would contaminate our observations, we created spectral energy distribution (SED) fits based on published *UBVRIJHK* photometric values obtained from the literature for each calibrator to establish diameter estimates. This also allowed us to see if there was any excess emission associated with a low-mass stellar companion or circumstellar disk. Calibrator candidates displaying variable radial velocities or any other indication of companions were discarded.

We used Kurucz model atmospheres⁸ based on $T_{\rm eff}$ and $\log g$ values to calculate limb-darkened angular diameters for the calibrators. The stellar models were fit to observed photometry after converting magnitudes to fluxes using Colina et al. (1996) for UBVRI values and Cohen et al. (2003) for JHK values. See Table 2 for the $T_{\rm eff}$ and $\log g$ used and the resulting limb-darkened angular diameters.

Available to download at http://kurucz.cfa.harvard.edu.

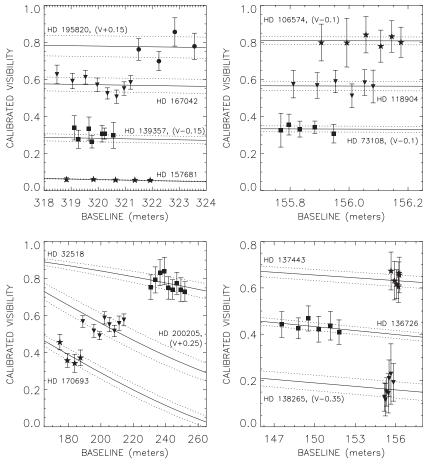


Figure 1. LD disk diameter fits for all the stars observed with one calibrator except HD 214868. The solid line represents the theoretical visibility curve for a star with the best-fit θ_{LD} , the dashed lines are the 1σ error limits of the diameter fit, the solid symbols are the calibrated visibilities, and the vertical lines are the measured errors. Some of the stars' visibilities were shifted as indicated by "(V \pm #)" so they would not overlap other data points.

4. DETERMINATION OF ANGULAR DIAMETER AND $T_{\rm eff}$

The observed quantity of an interferometer is defined as the visibility (V), which is fit to a model of a uniformly illuminated disk (UD) that represents the observed face of the star. Diameter fits to V were based upon the UD approximation given by $V = [2J_1(x)]/x$, where J_1 is the first-order Bessel function and $x = \pi B\theta_{\rm UD}\lambda^{-1}$, where B is the projected baseline at the star's position, $\theta_{\rm UD}$ is the apparent UD angular diameter of the star, and λ is the effective wavelength of the observation (Shao & Colavita 1992). A more realistic model of a star's disk involves limb-darkening (LD), and relationship incorporating the linear LD coefficient μ_{λ} (Hanbury-Brown et al. 1974) is

$$V = \left(\frac{1 - \mu_{\lambda}}{2} + \frac{\mu_{\lambda}}{3}\right)^{-1} \times \left[(1 - \mu_{\lambda}) \frac{J_{1}(x)}{x} + \mu_{\lambda} \left(\frac{\pi}{2}\right)^{1/2} \frac{J_{3/2}(x)}{x^{3/2}} \right].$$
 (1)

Table 3 lists the modified Julian Date (MJD), projected baseline (B) at the time of observation, projected baseline position angle (Θ), calibrated visibility (V_c), and error in V_c (σV_c) for each giant star observed. Figures 1–3 show the LD diameter fits for all the stars.

The LD coefficient was obtained from Claret et al. (1995) after adopting the $T_{\rm eff}$ and $\log g$ values required for each star observed. The resulting LD angular diameters are listed in Table 4. The average difference between the UD and LD diameters are on the

order of a few percent, and the final angular diameters are little affected by the choice of μ_{λ} . All but four stars have θ_{LD} errors of 2% or less, three of the four have errors of only 3%, and the final star has a 5% error. Additionally, the combination of the interferometric measurement of the star's angular diameter plus the *Hipparcos* parallax (van Leeuwen 2007a, 2007b) allowed us to determine the star's physical radius. The results are also listed in Table 4. In principle, one can calculate the mass of each star from the physical radius and $\log g$ values. However, the formal errors in $\log g$ lead to errors in such mass estimates near the 50% level, thereby significantly decreasing their usefulness to this analysis.

For each θ_{LD} fit, the errors were derived via the reduced χ^2 minimization method (Wall & Jenkins 2003; Press et al. 1992): the diameter fit with the lowest χ^2 was found and the corresponding diameter was the final θ_{LD} for the star. The errors were calculated by finding the diameter at $\chi^2 + 1$ on either side of the minimum χ^2 and determining the difference between the χ^2 diameter and $\chi^2 + 1$ diameter. In calculating the diameter errors in Table 4, we adjusted the estimated visibility errors to force the reduced χ^2 to unity because when this is omitted, the reduced χ^2 is well under 1.0, indicating we are overestimating the errors in our calibrated visibilities.

Limb-darkened angular diameters were estimated using the relationship described in Kervella et al. (2004) between the (V-K) color and log $\theta_{\rm LD}$ (see $\theta_{\rm estimate}$ in Table 1). The table also lists $R_{\rm estimate}$, which were derived using $\theta_{\rm estimate}$ and the stars' parallaxes. The major weakness of this method lies

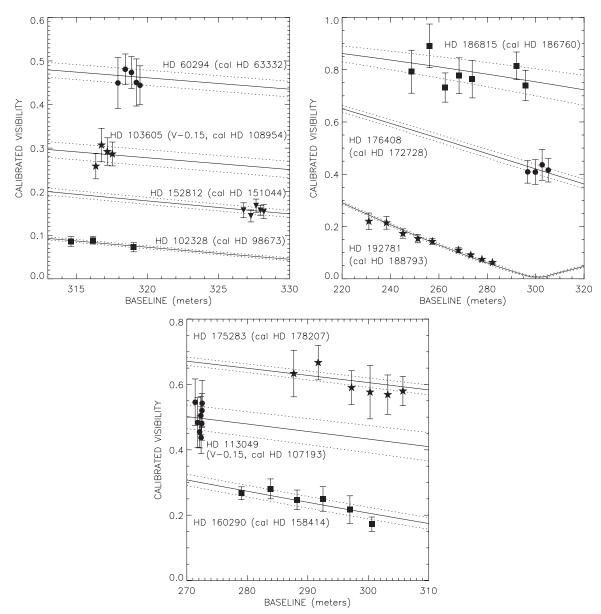


Figure 2. LD disk diameter fits for all the stars observed with two calibrators except HD 150010. The symbols are the same as listed in Figure 1. For the sake of clarity, the data points for one calibrator only are shown.

in the uncertainties surrounding the K-magnitudes, which were taken from two sources: the Two-Micron Sky Survey (TMSS; Neugebauer & Leighton 1969, errors $\sim 2\% -5\%$) and the 2MASS All-sky Catalog of Point Sources (2MASS; Cutri et al. 2003, errors $\sim 6\% -12\%$). Preference was given to the former because 2MASS measurements saturate at magnitudes brighter than ~ 3.5 in the K band even when using the shortest exposure time. The large errors associated with 2MASS magnitudes for these bright stars led to large errors in angular diameter and physical radii estimates.

Once $\theta_{\rm LD}$ was determined interferometrically, the $T_{\rm eff}$ was calculated using the relation

$$F_{\text{BOL}} = \frac{1}{4} \theta_{\text{LD}}^2 \sigma T_{\text{eff}}^4, \tag{2}$$

where $F_{\rm BOL}$ is the bolometric flux and σ is the Stefan-Boltzmann constant. The stars' V and K magnitudes were

dereddened using the extinction curve described in Cardelli et al. (1989) and interstellar absorption (A_V) values were from Famaey et al. (2005) except for HD 113049 and HD 176408, which had no A_V in the literature. A_V values for these two stars were estimated through a nonlinear, least squares fit and a reddening prescription from Fitzpatrick (1999), who presented a wavelength-dependent extinction curve. The intrinsic broadband color (V - K) was calculated and BCs were determined by interpolating between the [Fe/H] = +0.2, 0.0, and -1.0 tablesfound in Alonso et al. (1999). They point out that in the range of 6000 K $\geqslant T_{\rm eff} \geqslant$ 4000 K, their BC calibration is symmetrically distributed around a ± 0.10 mag band when compared to other calibrations. The average BC used here is 0.55, and because 0.10 is 18% of 0.55, we assigned a 18% error bar to our BC values. The bolometric flux was determined by applying the BC for each star and the $T_{\rm eff}$ was calculated (see Table 4). All $T_{\rm eff}$ errors are $\leq 4\%$, 11 stars have errors of $\leq 2\%$, and the major source of error in calculating $T_{\rm eff}$ stemmed, again, from uncertainties in K magnitudes.

⁹ Explanatory supplement to the 2MASS All Sky Data Release and Extended Mission Products, http://www.ipac.caltech.edu/2mass/releases/allsky/doc/.

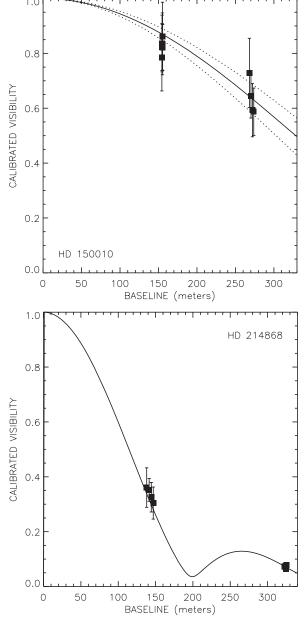


Figure 3. LD disk diameter fits for HD 150010 (top panel) and HD 214868 (bottom panel). The symbols are the same as listed in Figure 1.

Giant star masses were estimated using the PARAM stellar model 10 from Girardi et al. (2000) with a modified version of the method described in da Silva et al. (2006). The input parameters for each star were its interferometrically measured $T_{\rm eff}$, its spectroscopically derived [Fe/H], its V magnitude from Mermilliod (1991), and its Hipparcos parallax (van Leeuwen 2007a, 2007b) along with the corresponding error for each value. The model used these inputs to estimate each star's age, mass, radius, $(B-V)_0$, and $\log g$ using the isochrones and a Bayesian estimating method, calculating the probability density function separately for each property in question. da Silva et al. qualify mass estimates as "more uncertain" than other properties, so the resulting masses listed in Table 1 should be viewed as rough estimates only.

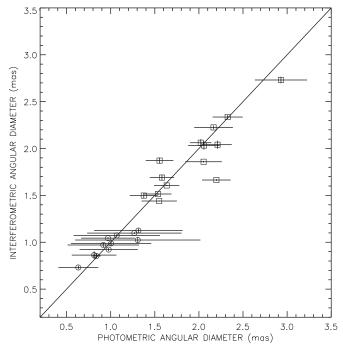


Figure 4. Comparison of photometrically estimated and interferometrically measured diameters. The squares and circles represent diameters estimated using K magnitudes from TMSS and 2MASS, respectively, and the diagonal solid line indicates a 1:1 ratio for the diameters. Note the significantly larger error bars associated with the photometric diameters, particularly those using 2MASS data. The outliers above and below the line are HD 118904 and HD 157681, respectively, and the discrepancies may be due to the calibrator used (see Section 5 for more details).

5. RESULTS AND DISCUSSION

In order to check how well the estimated and measured angular diameters agreed, we plotted photometrically estimated versus interferometrically measured angular diameters in Figure 4, and Figure 5 shows a similar plot for physical radii. The angular diameters determined using K-band photometry from 2MASS show generally higher errors in Figure 4 than the diameters determined using TMSS photometry. This plot clearly shows the advantage of measuring angular diameters interferometrically, as the errors are significantly smaller than the photometric estimates in all cases. There is an even scatter around the 1:1 ratio line, and all but two stars are within 1σ of the line.

The outliers in both Figures 4 and 5 are HD 118904 and HD 157681. Neither star shows any sign of binarity in the literature, and the SEDs created using the $T_{\rm eff}$ and log g based on their spectral type and Cox (2000) do not show any excess in the infrared wavelengths that would suggest a low-mass stellar companion or a circumstellar disk. In both cases, the problem may lie with the calibrator stars chosen. HD 157681 was observed using the calibrator HD 158460, and though the latter has a small estimated diameter (0.268 \pm 0.016 mas) and its SED shows no excess flux in the infrared that would indicate a low-mass stellar companion or circumstellar disk, HD 157681 was the only star observed with that calibrator and there could be an unseen companion that is not taken into account when estimating the star's diameter. Future observations of HD 157681 with different calibrators will make the situation clearer.

HD 118904 was observed using HD 124063 as a calibrator, and the same calibrator was used to observe the target star HD 113049 along with the second calibrator HD 107193. When

http://stev.oapd.inaf.it/cgi-bin/param_1.0

 Table 4

 Interferometric Diameter and Effective Temperature Measurements of the K Giants

Target HD	$ heta_{ ext{UD,interferometric}}$ (mas)	$ heta_{ ext{LD,interferometric}}$ (mas)	σ _{LD} (%)	$R_{ m linear}$ (R_{\odot})	$A_{ m V}$	ВС	L_{\star} (L_{\odot})	F_{BOL} (10 ⁻⁸ erg s ⁻¹ cm ⁻²)	T _{eff} (K)	σ _{Teff} (%)
32518	0.828 ± 0.022	0.851 ± 0.022	3	11.04 ± 0.77	0.06	0.43 ± 0.08	49.2 ± 3.6	10.8 ± 0.9	4600 ± 112	2
60294	1.014 ± 0.010	1.044 ± 0.010	1	9.17 ± 0.29	0.05	0.35 ± 0.06	32.5 ± 1.9	15.6 ± 1.0	4552 ± 74	2
73108	2.161 ± 0.019	2.225 ± 0.020	1	18.79 ± 0.38	0.00	0.51 ± 0.09	112.4 ± 10.0	58.3 ± 5.2	4336 ± 99	2
102328	1.546 ± 0.006	1.606 ± 0.006	0.4	11.42 ± 0.23	0.00	0.51 ± 0.09	42.4 ± 3.8	31.0 ± 2.8	4358 ± 97	2
103605	1.066 ± 0.009	1.098 ± 0.010	1	11.20 ± 0.41	0.00	0.52 ± 0.09	52.9 ± 4.8	18.8 ± 1.7	4651 ± 109	2
106574	1.458 ± 0.027	1.498 ± 0.028	2	23.02 ± 0.92	0.00	0.54 ± 0.10	136.6 ± 12.7	21.4 ± 2.0	4113 ± 105	3
113049a	0.945 ± 0.021	0.971 ± 0.022	2	17.35 ± 1.07	0.00	0.35 ± 0.06	119.7 ± 7.2	13.9 ± 0.9	4583 ± 93	2
118904	1.842 ± 0.031	1.871 ± 0.032	2	25.38 ± 0.88	0.00	0.60 ± 0.11	136.0 ± 14.1	27.3 ± 2.9	3913 ± 108	3
136726	2.264 ± 0.020	2.336 ± 0.020	1	30.68 ± 0.76	0.04	0.70 ± 0.13	229.2 ± 28.2	49.2 ± 6.1	4055 ± 126	3
137443	1.638 ± 0.030	1.690 ± 0.031	2	20.51 ± 0.62	0.06	0.68 ± 0.12	96.1 ± 11.5	24.1 ± 2.9	3990 ± 125	3
138265	1.998 ± 0.037	2.062 ± 0.038	2	43.40 ± 2.75	0.06	0.95 ± 0.17	337.8 ± 57.5	28.2 ± 4.9	3758 ± 166	4
139357	1.040 ± 0.012	1.073 ± 0.013	1	13.63 ± 0.51	0.13	0.40 ± 0.07	73.6 ± 5.1	16.9 ± 1.2	4580 ± 86	2
150010	0.995 ± 0.028	1.024 ± 0.029	3	15.84 ± 1.08	0.04	0.70 ± 0.13	98.9 ± 12.2	15.3 ± 1.9	4572 ± 158	3
152812	1.393 ± 0.003	1.440 ± 0.004	0.3	31.16 ± 2.82	0.10	0.72 ± 0.13	270.5 ± 34.4	21.4 ± 2.9	4193 ± 142	3
157681	1.600 ± 0.009	1.664 ± 0.010	1	34.22 ± 1.78	0.04	0.94 ± 0.17	381.7 ± 64.4	33.4 ± 5.7	4361 ± 187	4
160290	1.467 ± 0.010	1.515 ± 0.010	1	17.65 ± 0.42	0.10	0.50 ± 0.09	114.4 ± 9.5	31.2 ± 2.7	4493 ± 98	2
167042	0.898 ± 0.017	0.922 ± 0.018	2	4.98 ± 0.07	0.01	0.39 ± 0.07	11.7 ± 0.8	14.8 ± 1.0	4785 ± 93	2
170693	1.981 ± 0.041	2.041 ± 0.043	2	21.19 ± 0.60	0.02	0.59 ± 0.11	149.7 ± 15.3	51.4 ± 5.3	4386 ± 122	3
175823	0.958 ± 0.022	0.988 ± 0.023	2	18.88 ± 1.04	0.05	0.49 ± 0.09	132.7 ± 11.3	13.4 ± 1.2	4509 ± 113	3
176408	1.092 ± 0.022	1.125 ± 0.023	2	10.24 ± 0.23	0.02	0.49 ± 0.09	49.2 ± 4.2	21.9 ± 1.9	4775 ± 113	2
186815	0.713 ± 0.020	0.731 ± 0.020	3	6.11 ± 0.25	0.02	0.21 ± 0.04	18.2 ± 0.7	9.6 ± 0.4	4823 ± 81	2
192781	1.787 ± 0.002	1.859 ± 0.003	0.2	35.57 ± 1.46	0.40	0.62 ± 0.11	405.2 ± 43.8	40.9 ± 4.5	4342 ± 119	3
195820	0.840 ± 0.040	0.863 ± 0.041	5	10.69 ± 0.62	0.07	0.33 ± 0.06	50.6 ± 2.8	12.2 ± 0.7	4707 ± 131	3
200205	1.963 ± 0.043	2.032 ± 0.045	2	41.23 ± 2.08	0.69	0.59 ± 0.11	569.9 ± 58.6	51.2 ± 5.4	4392 ± 125	3
214868	2.721 ± 0.020	2.731 ± 0.024	1	29.98 ± 0.84	0.15	0.69 ± 0.12	286.9 ± 34.9	88.1 ± 10.8	4339 ± 134	3

Note. ^a The angular diameter and subsequent calculations are based on data calibrated using HD 107193 only. See Section 5 for more details.

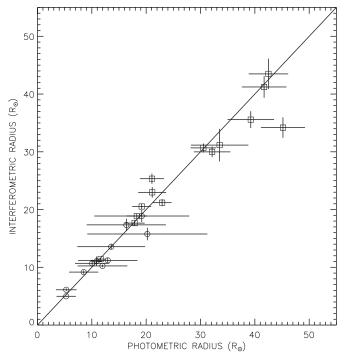


Figure 5. Comparison of photometrically and interferometrically determined linear radii. The symbols and outliers are the same as listed in Figure 4.

the data were calibrated separately for HD 113049, the diameters showed a 0.08 mas difference, which is on the order of an 8% change. If HD 118904's diameter is reduced by 8%, the data point is within errors on the 1:1 ratio line for both plots in Figures 4 and 5. Because this is the case, only HD 107193 was

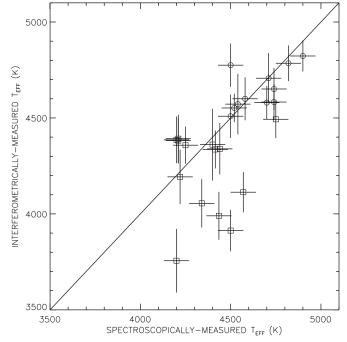


Figure 6. Comparison of spectroscopically and interferometrically measured effective temperatures. The symbols are the same as listed in Figure 4.

used in the calibration of HD 113049's data, and the angular diameter, radius, and $T_{\rm eff}$ listed in Table 4 are based on those data alone.

Figure 5 shows that while a fair number of photometric and interferometric radii agree very well, there are some that show slight discrepancies, notwithstanding the error bars. This could

be due to a few different effects. First, the photometrically determined radii depend on temperature estimates that may not be correct. If the star is highly active or there is a very faint companion, these could affect the temperature and therefore radii estimates. Second, the LD law used to determine interferometric diameters and radii may not take certain stellar features into account, such as starspots or extremely active regions. This would not be a large effect because even altering the LD coefficient μ_{λ} by 20% changes the limb-darkened angular diameter by an average of 0.7%. Third, the differences may be due to changes in the stars' convections zones, because as the star evolves the convection zone gets deeper. Convection is not well modeled, which may lead to errors in the photometric radii estimates.

We also plotted the interferometrically measured $T_{\rm eff}$ versus those derived spectroscopically in Figure 6. There is some scatter off the 1:1 ratio line, particularly for the cooler stars. The errors in $T_{\rm eff}$ do not show a trend with log g, diameter, radius, (V-K) color, distance, spectral type, metallicity, or BC. The discrepancies may be due to the inherent properties of the methods used to measure $T_{\rm eff}$. Spectroscopic values are based on Fe I and Fe II lines and measure the $T_{\rm eff}$ in the part of the atmosphere where those lines are present, while interferometry calculates the overall $T_{\rm eff}$ of the star using the measured diameter. It has been surmised that atmospheric models of K giant stars in the near-ultraviolet band are missing a source of thermal extinction, which would also affect the $T_{\rm eff}$ measurements (Short & Hauschildt 2009).

Our next step will be to determine the oscillation frequencies of these stars so that we can compare the true masses of these stars with those estimated using evolutionary models.

Many thanks to Douglas Gies for his help and advice. The CHARA Array is funded by the National Science Foundation through NSF grant AST-0606958 and by Georgia State University through the College of Arts and Sciences, and S.T.R. acknowledges partial support by NASA grant NNH09AK731. We are also grateful to the user support group of the Alfred-Jensch telescope. This research has made use of the SIMBAD database, operated at CDS, Strasbourg, France. This publication makes use of data products from the 2MASS, which is a joint project of the University of Massachusetts and the Infrared Processing and Analysis Center/California Institute of Technology, funded by the National Aeronautics and Space Administration and the National Science Foundation.

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 $^{^{11}}$ If a second star is present and is more than \sim 2.5 mag fainter than the host star, the effects of the secondary star will be not seen in interferometric observations and would therefore have no effect on the angular diameter or physical radii measurements.